

Mechanically Efficient Cellular Microstructures in Plants

Lorna J. Gibson

Materials Science & Engineering

MIT

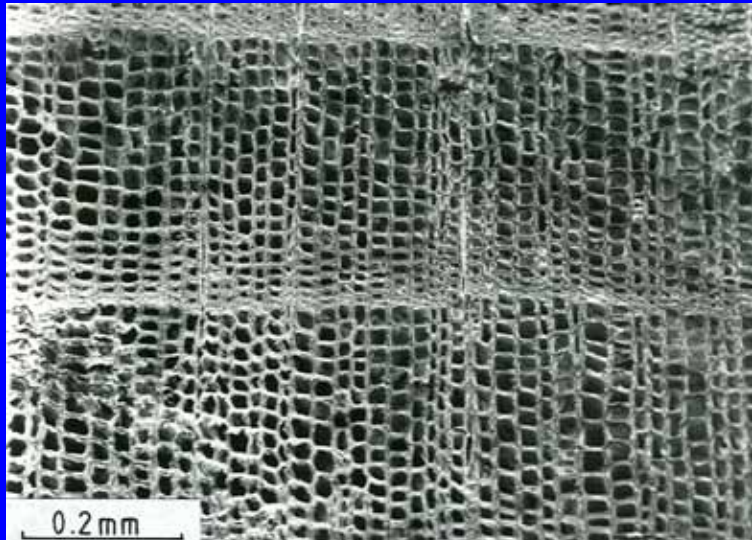
Introduction

- Plants are typically loaded in bending by wind and in compression by self-weight
- Minimizing mass reduces metabolic cost to grow material
- Examine strategies used in plants to reduce mass

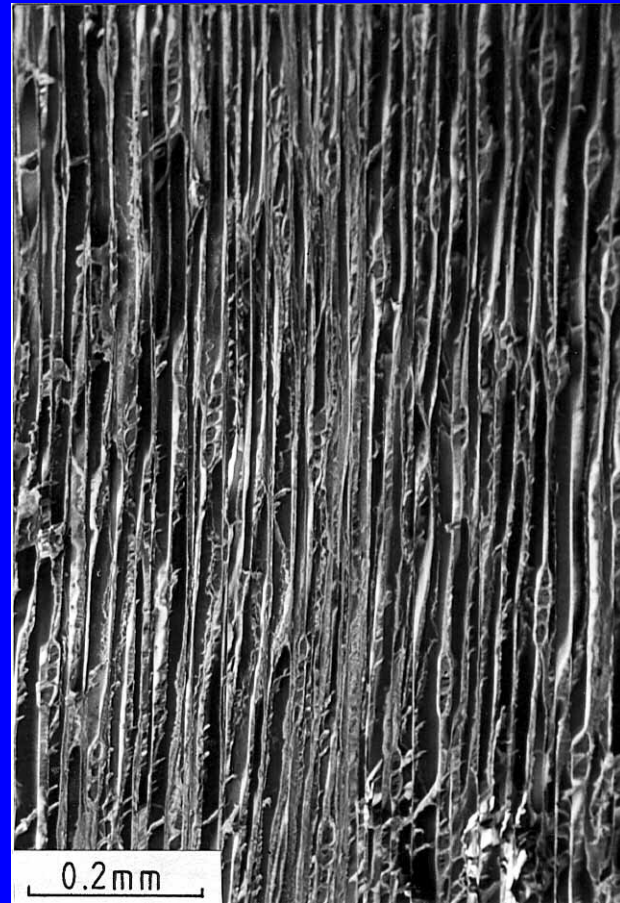
Introduction

- *Wood*: Uniform honeycomb-like structure
- *Palm stem*: Radial density gradient
- *Plant stem*: Cylindrical shell with compliant core
- *Monocotyledon leaves*: Sandwich structures

Wood: Honeycomb-Like Microstructure



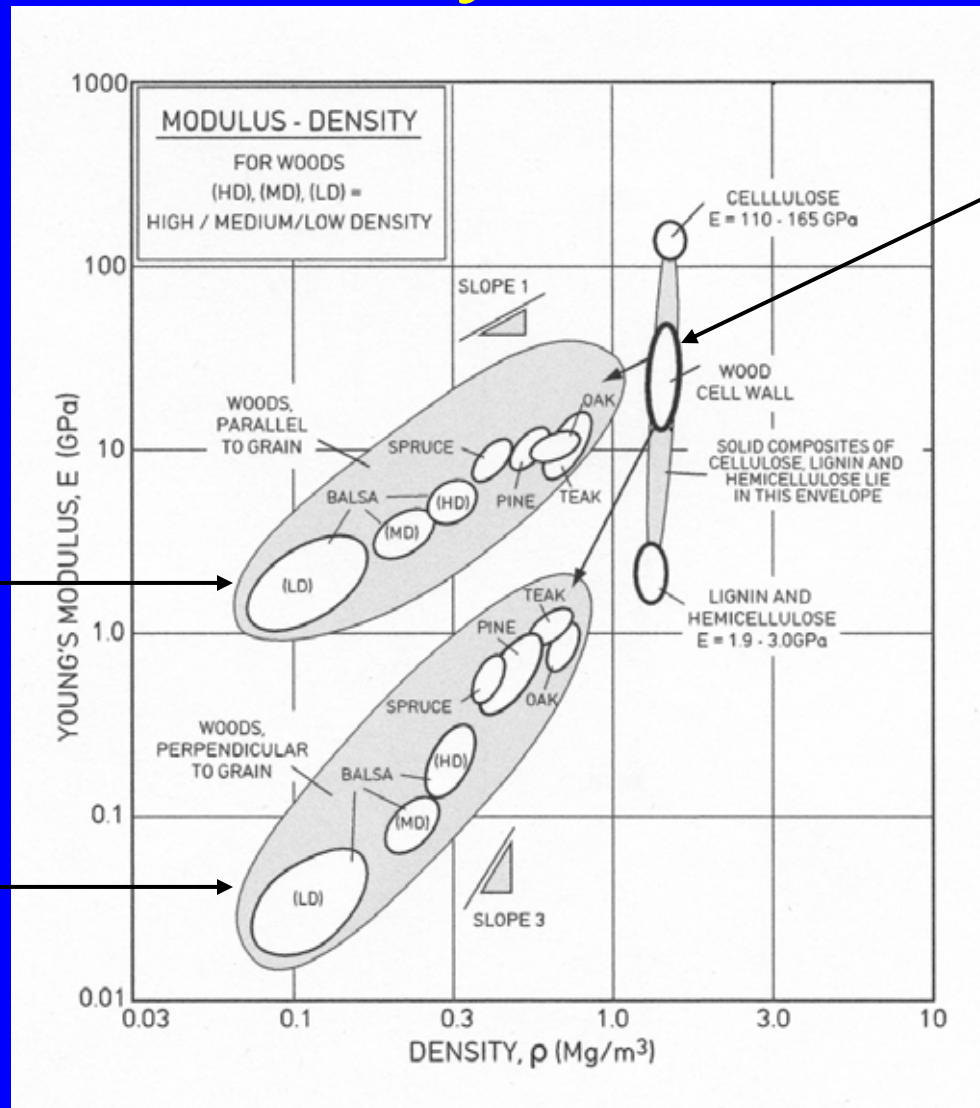
Cedar



Wood: Honeycomb Models

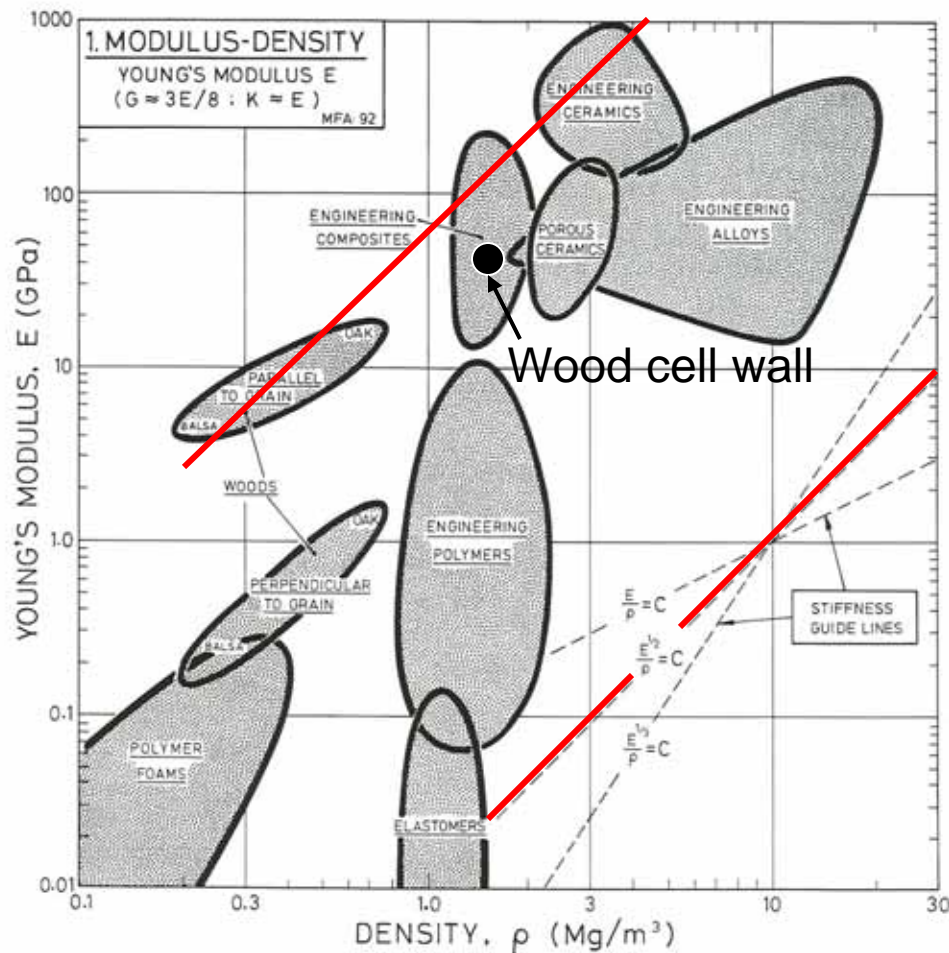
$$\frac{E^*}{E_{s\text{ along}}} = \frac{\rho^*}{\rho_s}$$

$$\frac{E^*}{E_{s\text{ across}}} = \left(\frac{\rho^*}{\rho_s} \right)^3$$



Cell wall:
Fiber
Composite
Model

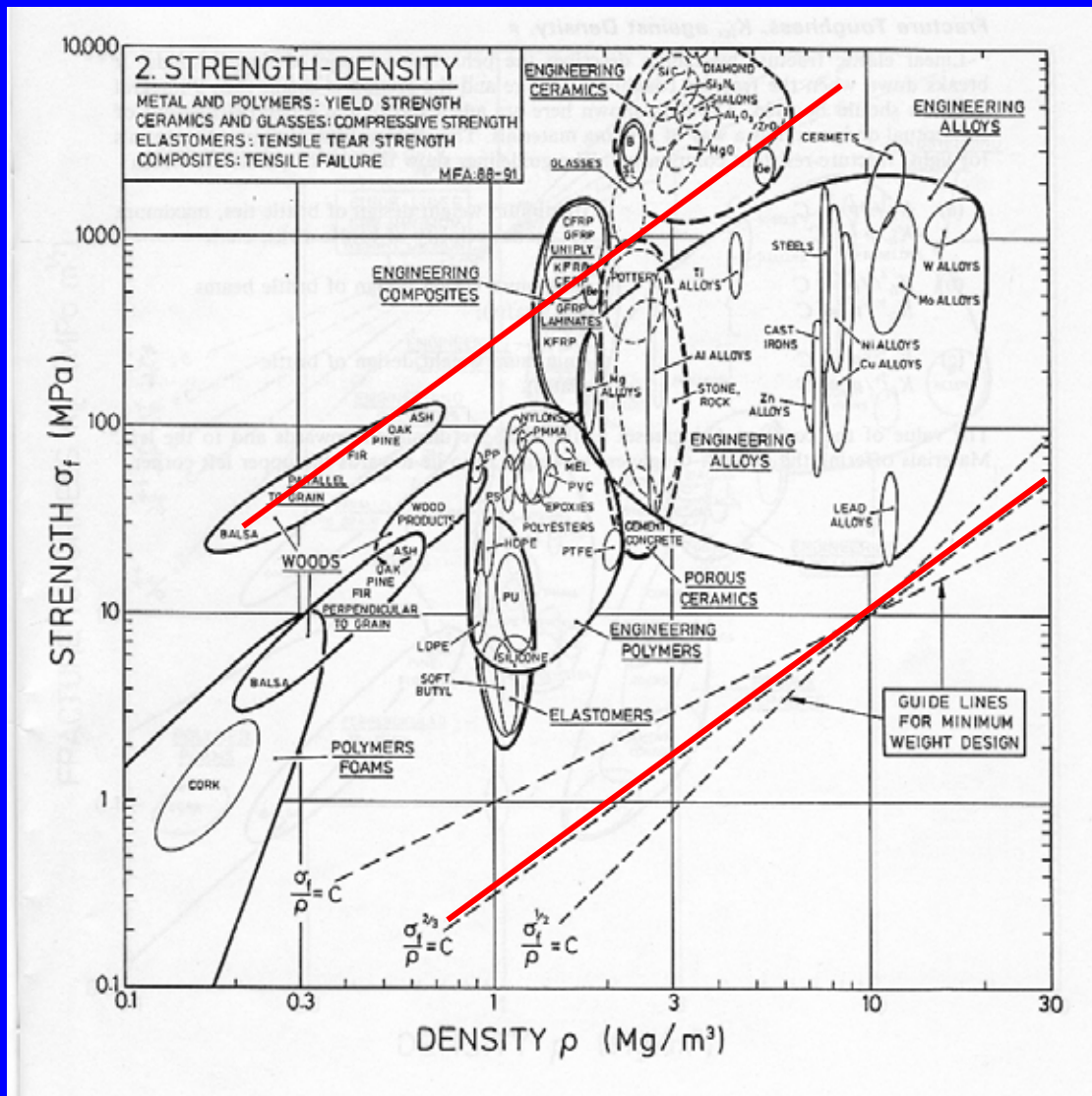
Wood in Bending: $E^{1/2}/\rho$



$$\frac{(E^*)^{1/2}}{\rho^*} = \frac{(E_s)^{1/2}}{\rho_s} \left(\frac{\rho_s}{\rho^*} \right)^{1/2}$$

Stiffness performance index for wood in bending is similar to that for best engineering composites

Wood in Bending: $\sigma_f^{2/3}/\rho$



$$\frac{(\sigma_f^*)^{2/3}}{\rho^*} = \frac{(\sigma_{ys})^{2/3}}{\rho_s} \left(\frac{\rho_s}{\rho^*} \right)^{1/3}$$

Strength performance index for wood in bending is similar to that for best engng composites

Wood

- Tree in bending loaded as cantilever
- Radius decreases with distance away from the ground
- Further increases mechanical performance of the tree
- $E = \text{constant}$, $r = r(z)$

Palm Stem: Radial Density Gradient

(Also Bamboo)

Palm Stem: A Different Strategy

- Stem has constant diameter: $r = \text{constant}$
- As palm grows taller, it increases the density of the material towards its periphery
- Cell wall thickness increases towards periphery of stem and towards the base of the stem $E = E(r, z)$

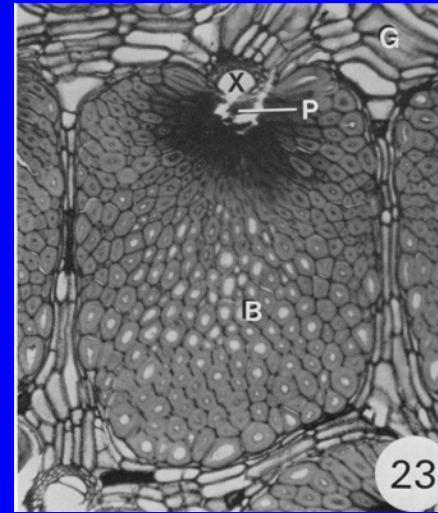
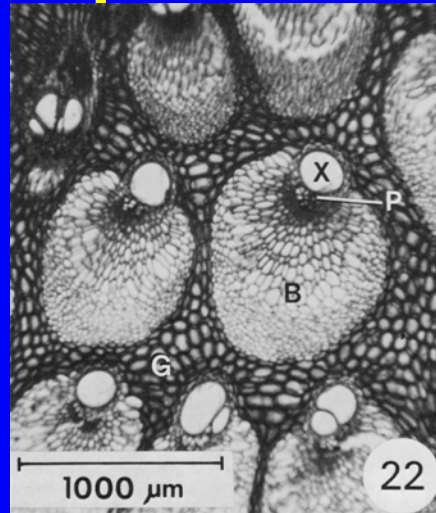


Coconut Palm

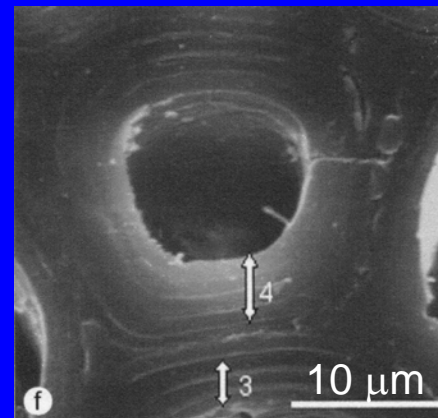
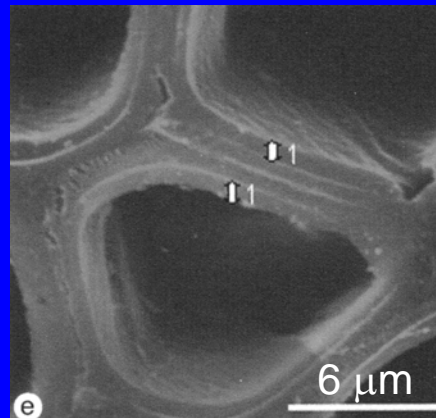
<http://en.wikipedia.org/wiki/>

Image:Palmtree_Curacao.jpg

Palm: Microstructure of Peripheral Stem Tissue



Rich, 1987

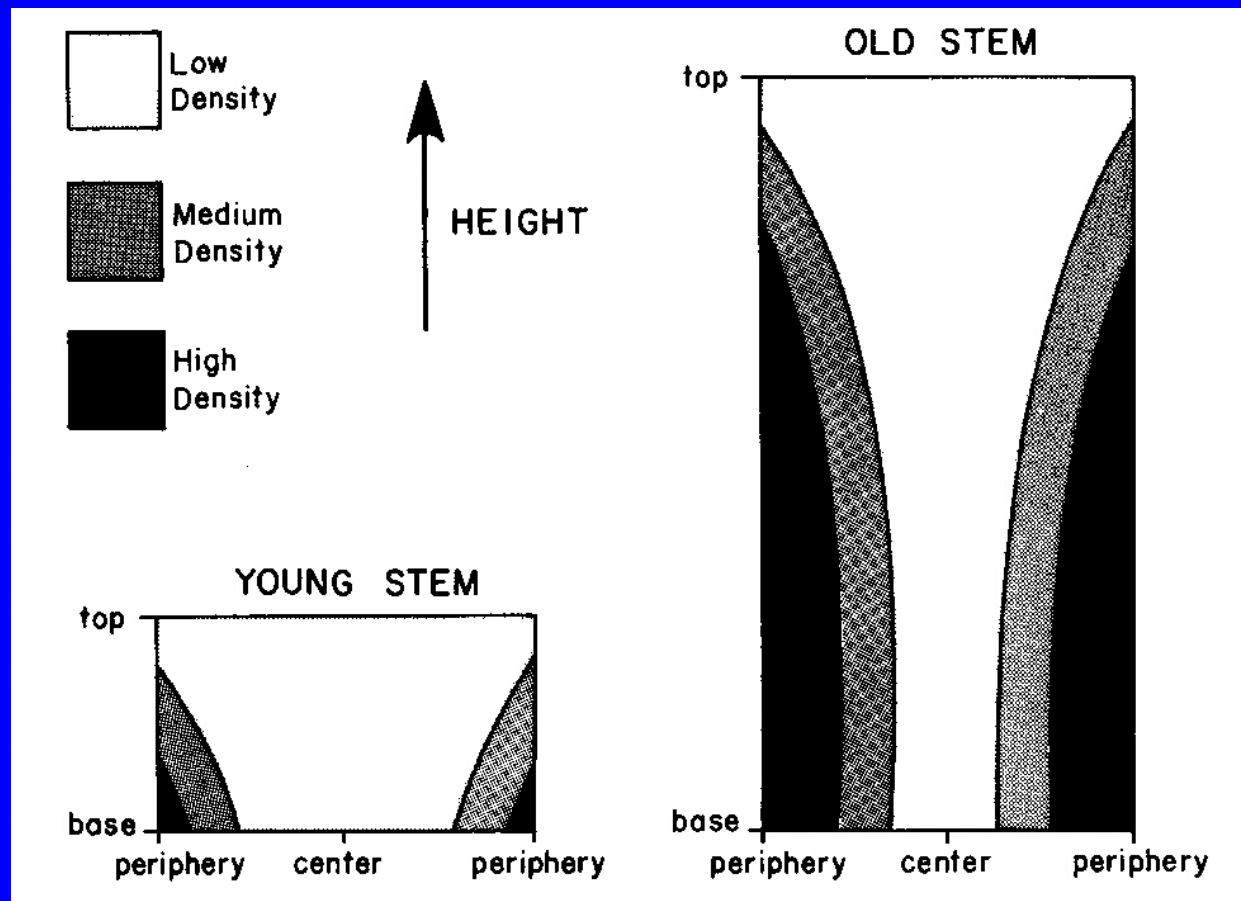


Kuo-Huang et al., 2004

Young

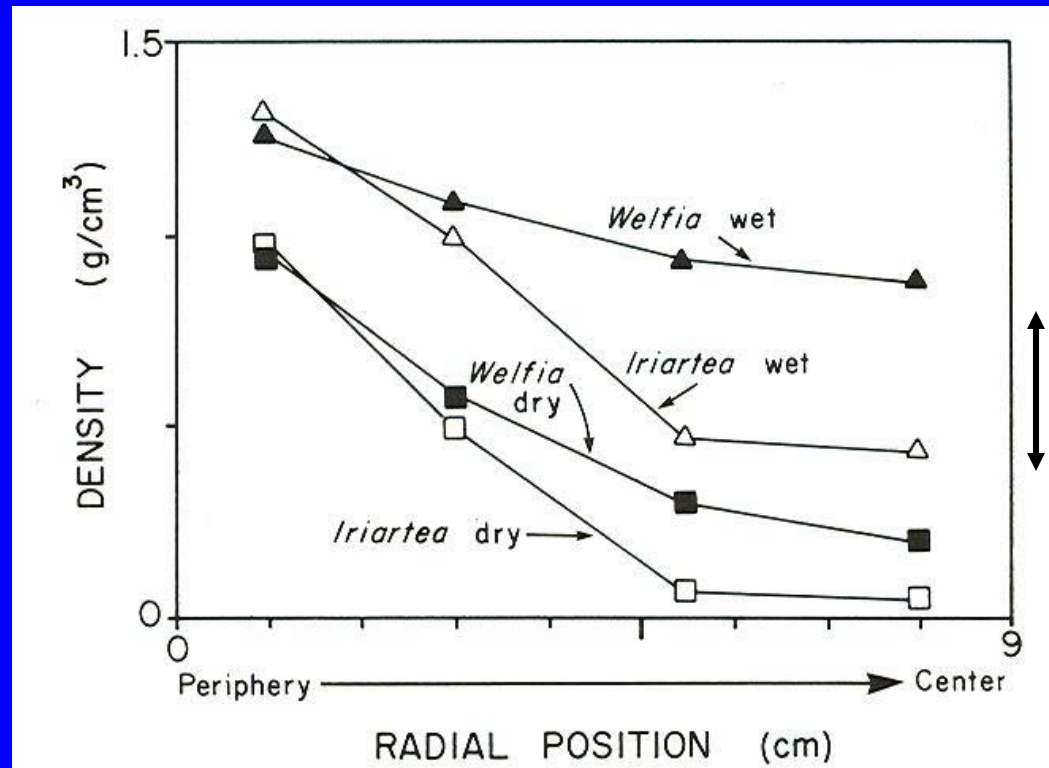
Old

Palm Stem: Density Gradient



Rich, PM (1987) Bot. Gazette 148, 42-50.

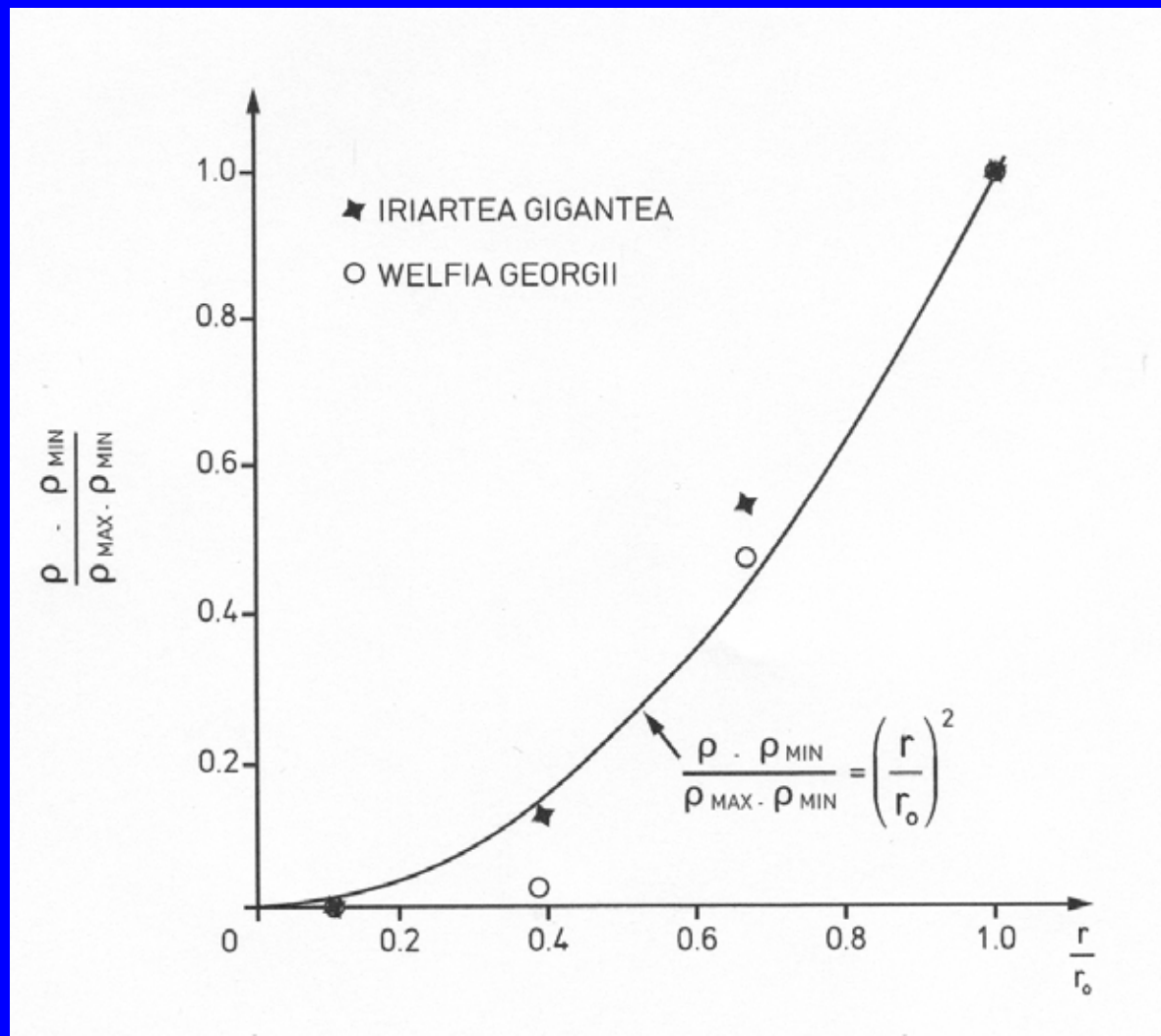
Palm Stem: Density at Breast Height



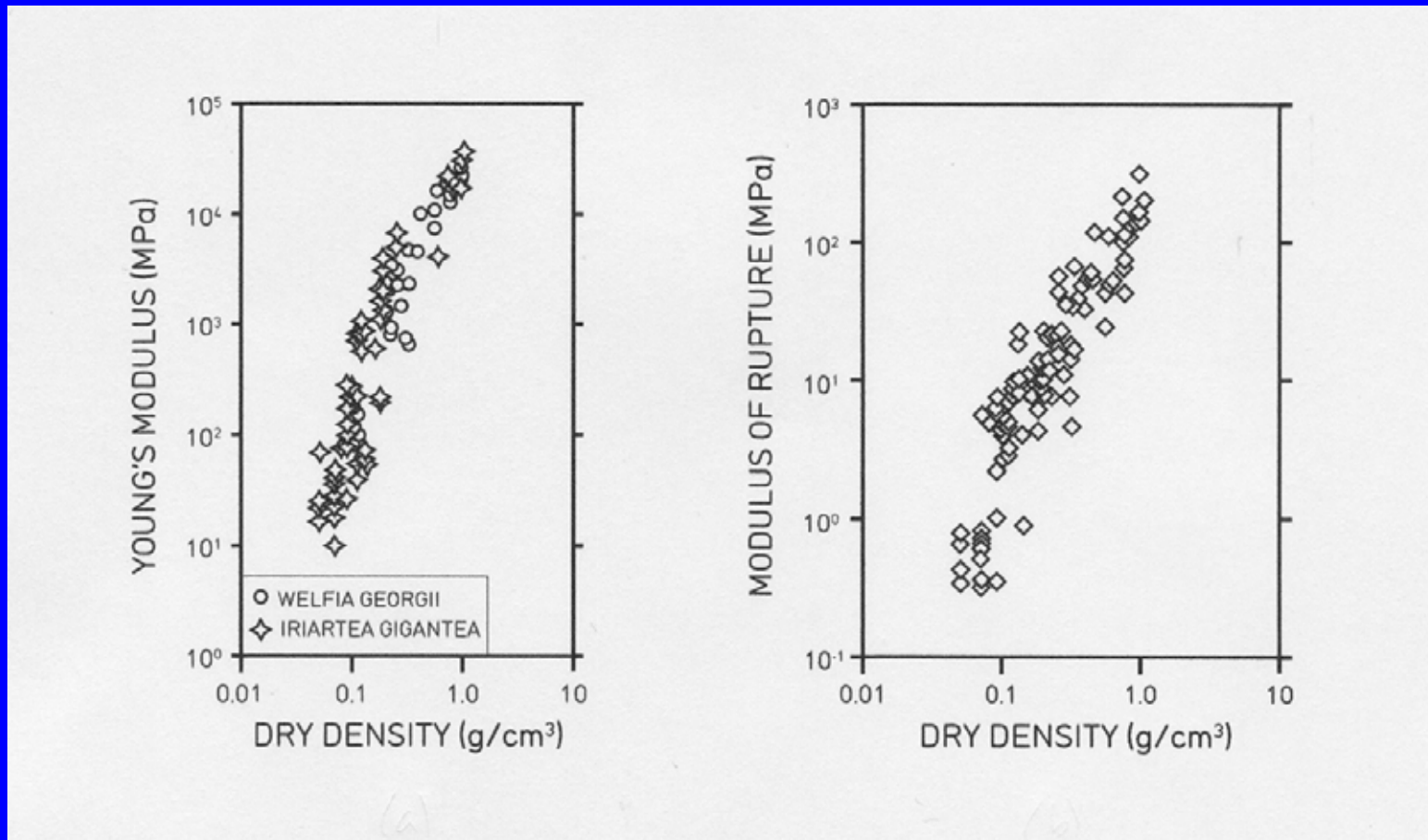
Densities
of common
woods

A single mature palm has a similar range of density as nearly all species of wood combined

Palm Stem: Density Gradient



Palm Stem: Mechanical Properties vs. Density



Rich, PM (1987) Bot. Gazette 148, 42-50.

Density Gradient: *Iriartea gigantea*

$$\rho = \left(\frac{r}{r_o} \right)^n \rho_{\max}$$

$$(EI)_{\text{gradient}} = \frac{C \pi r_o^4}{mn + 4}$$

$$E = C \left(\frac{\rho}{\rho_{\max}} \right)^m = C \left(\frac{r}{r_o} \right)^{mn}$$

$$\frac{(EI)_{\text{gradient}}}{(EI)_{\text{uniform}}} = \frac{4}{mn + 4} \left(\frac{n + 2}{2} \right)^m$$

Iriartea palm: $n = 2$, $m = 2.5$, $(EI)_{\text{gradient}} / (EI)_{\text{uniform}} = 2.5$

Similar calculation for *Welfia georgii*, gives

$$(EI)_{\text{gradient}} / (EI)_{\text{uniform}} = 1.6$$

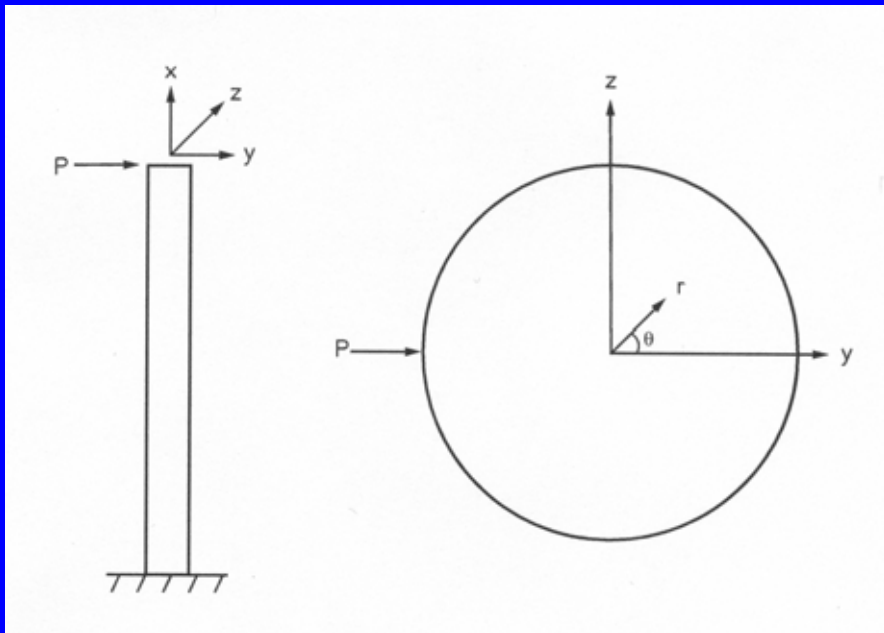
Palm Stem: Bending Stress Distribution

$$\sigma(y) = E\varepsilon = EKy$$

$$\sigma(r, \theta) = C \left(\frac{r}{r_o} \right)^{mn} \kappa r \cos \theta \propto r^{mn+1}$$

Iriarteia gigantea: $m = 2.5$, $n = 2$

$$\sigma \propto r^6$$



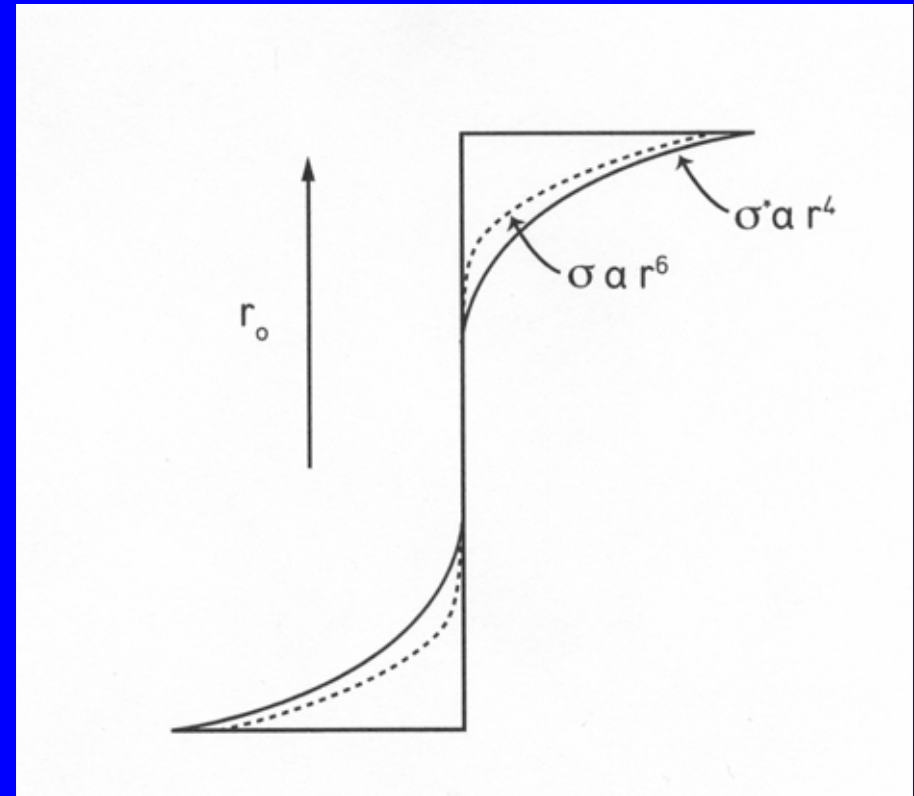
Palm Stem: Bending Strength Distribution

$$\sigma^* \propto \left(\frac{\rho}{\rho_{\max}} \right)^q \propto \left(\frac{r}{r_o} \right)^{nq}$$

Iriartea gigantea: $n = 2, q = 2$

$$\sigma^* \propto r^4$$

Strength matches
bending stress distribution



Plant Stems:
Cylindrical Shells with
Compliant Cores

(Also in Animal Quills,
Toucan Beak)

Plant Stems

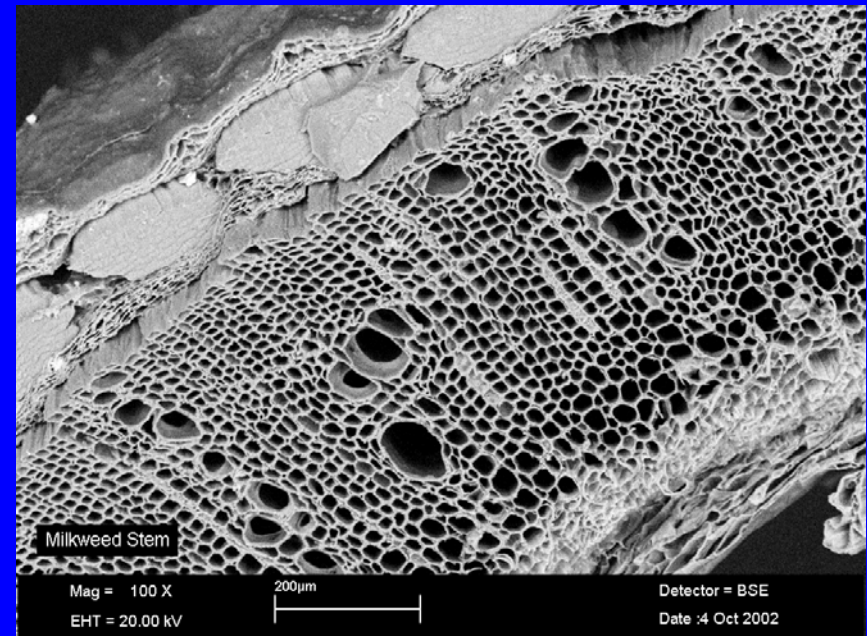
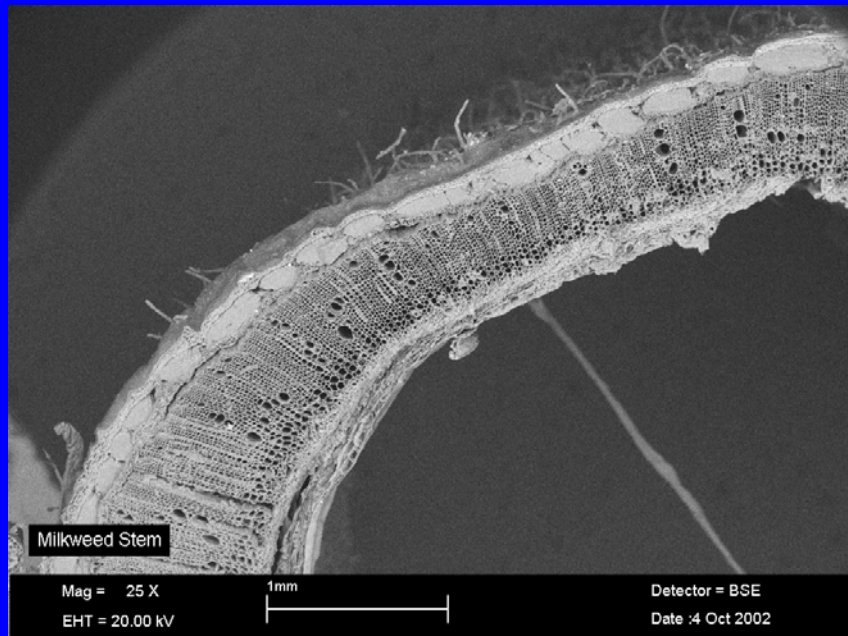


Milkweed

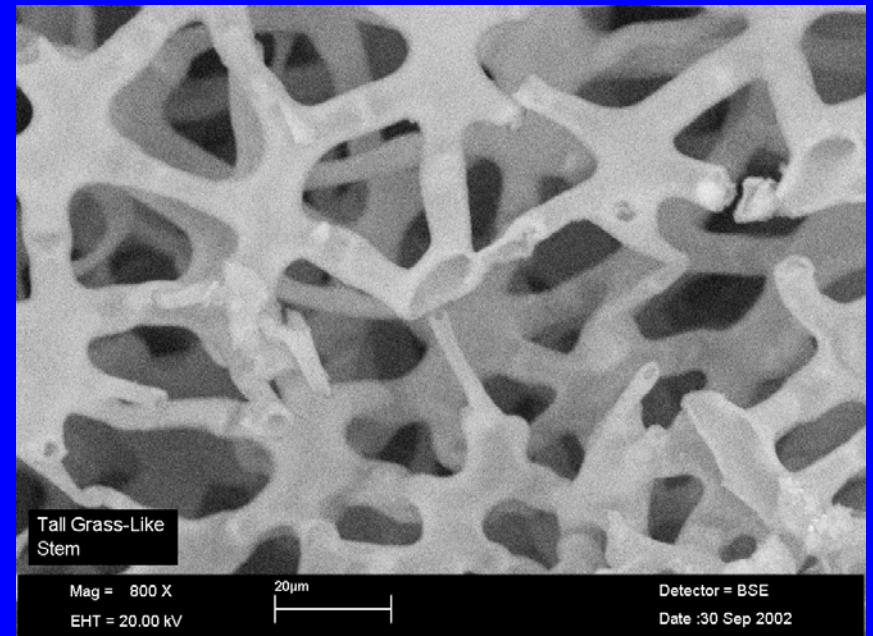
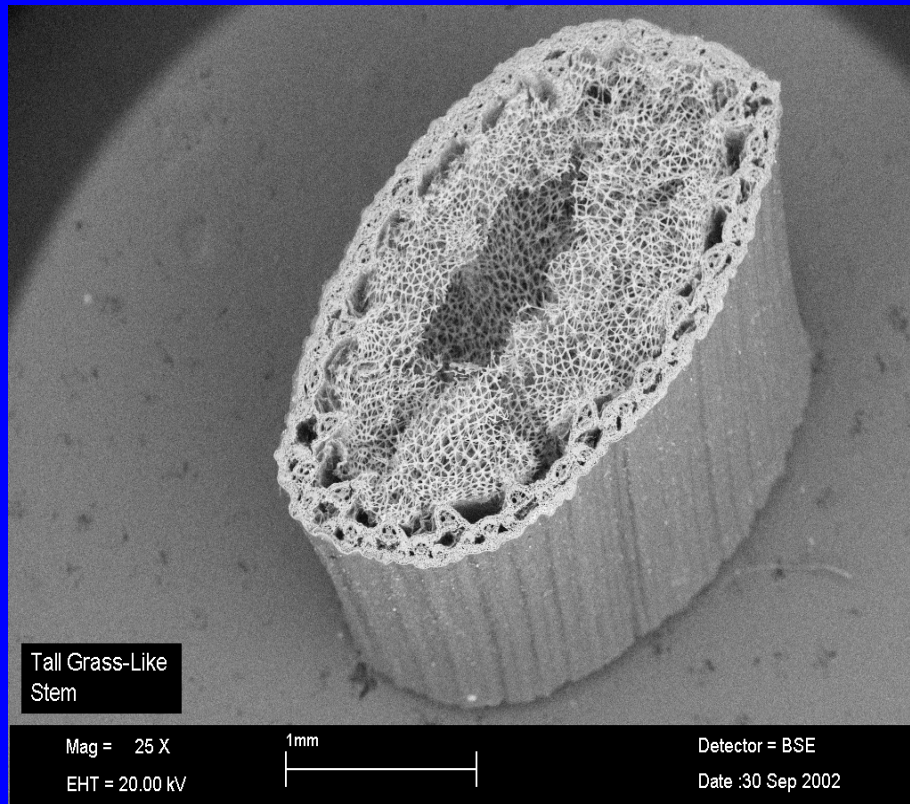


Grassy stem

Milkweed Stem



Grassy Stem



Hollow struts

Plant stems

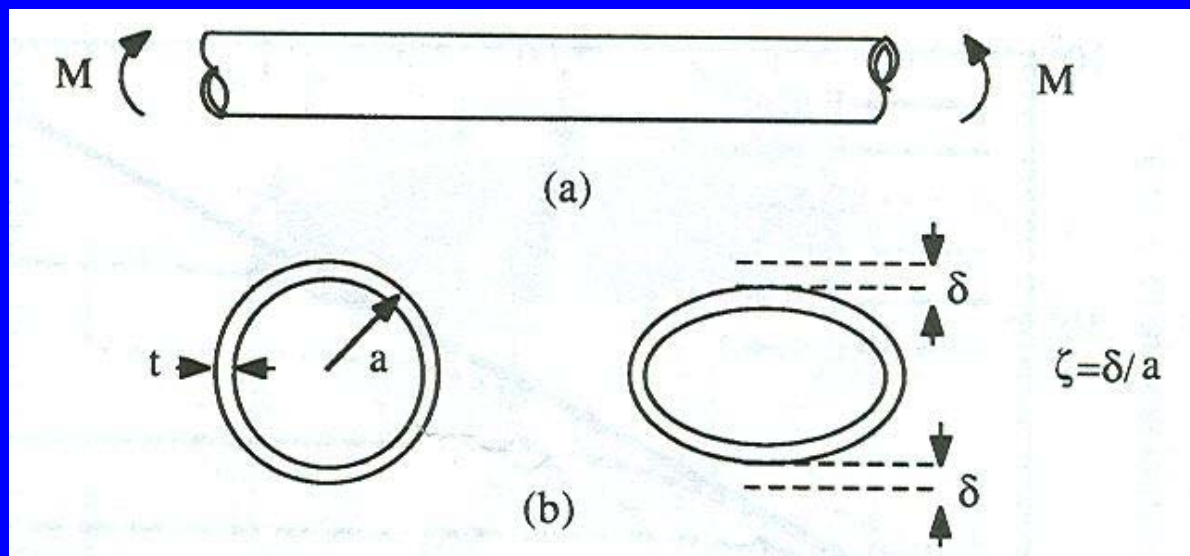
- Circular tube cross-section
- Resists bending (wind loads)
- Maximize shape factor

$$\Phi = \frac{4\pi I}{A^2} = \frac{a}{t}$$

- Maximize a/t , but limited by local buckling and ovalization
- Plant stems have compliant core (“core-rind structure”)

Plant Stems: Bending

- Core resists ovalization and increases local buckling resistance



Plant Stems: Bending

- Local buckling occurs when normal stress in compressive side of cylinder equals critical stress for axisymmetric buckling under uniaxial stress

- Hollow cylinder:

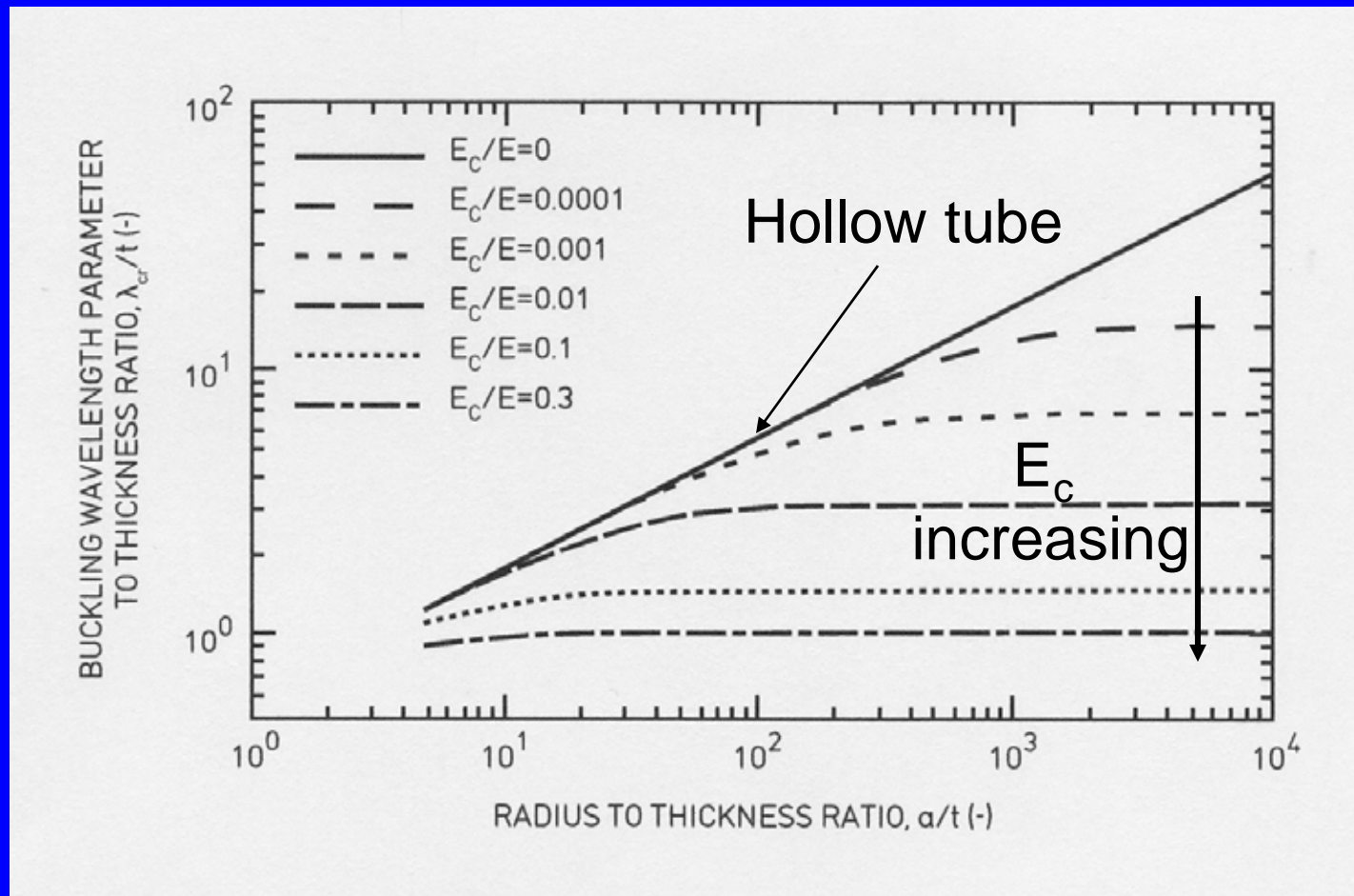
$$M_{lb} = \frac{0.939Eat^2}{\sqrt{1-\nu^2}}$$

- Cylinder with compliant core:

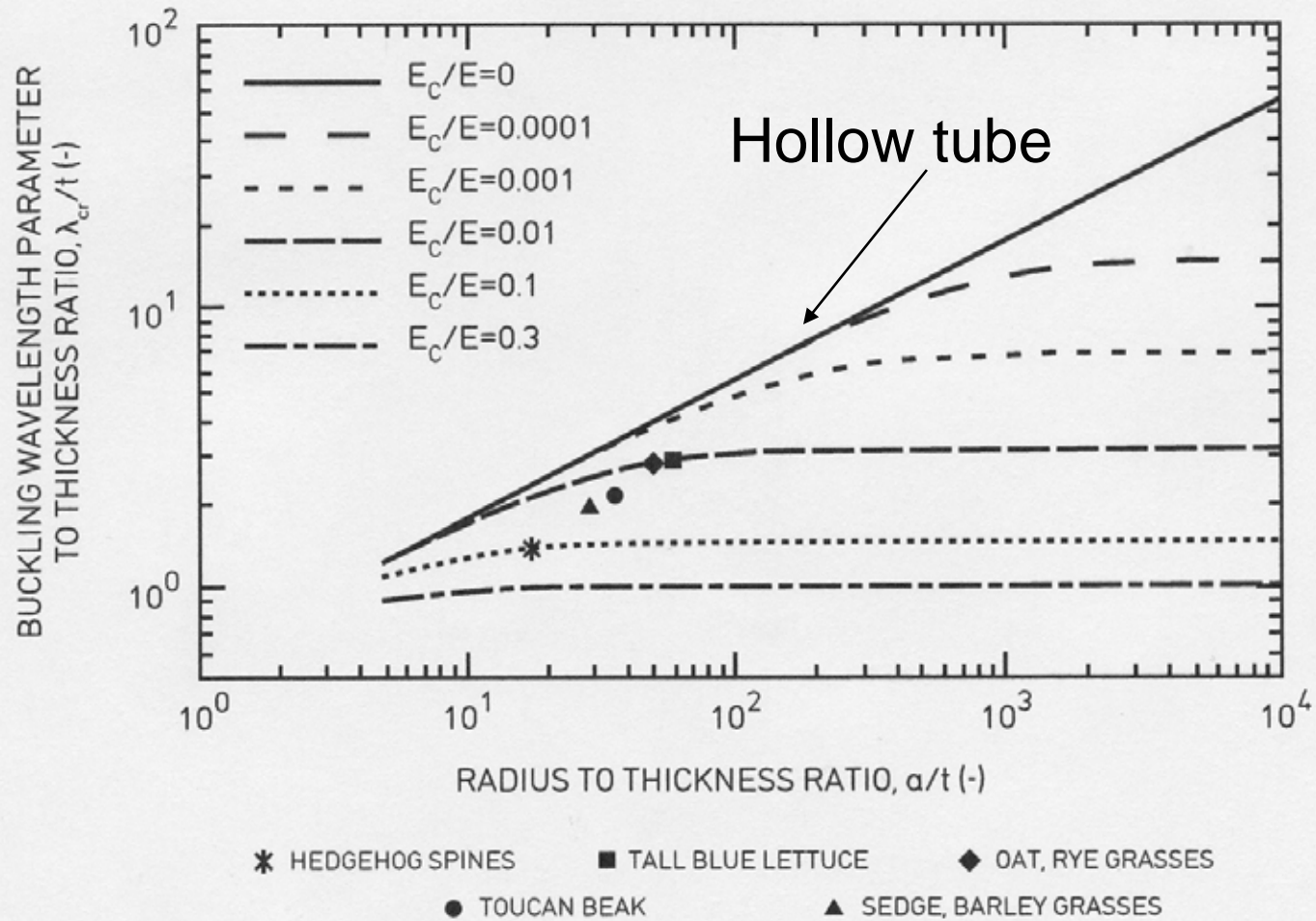
$$M_{lb} = \frac{\pi Ea^2t}{\sqrt{1-\nu^2}} f \left\{ \frac{\delta}{r}, \frac{E_{core}}{E_{shell}}, \frac{a}{t} \right\}$$

Plant Stems

- Foam-like core can act like elastic foundation supporting outer shell, increasing local buckling moment, M_{lb} , reducing buckling λ



Plant Stems



Plant Stems

- Within the core stress decays as move radially inward, away from the shell
- Stresses less than 5% of maximum at a radial distance of $5\lambda_{cr}$
- Can remove inner core, leaving core thickness, $c = 5\lambda_{cr}$

Plant Stems

Species	a/t	Elastic foundation	M_{lb}/M_{eq}	c/λ_{cr}
Tall blue lettuce	59	Yes	1.37	3.81
Oat, rye grasses	50	Yes	1.26	3.81
Sedge grass, common barley	25	Yes	0.77	3.27

Core increases buckling resistance for high a/t

Monocotyledon Leaves: Sandwich Structures

(Also in Skulls, Cuttlefish
Bone, Horseshoe Crab Shell)

Monocotyledon Leaves: Sandwich Beams

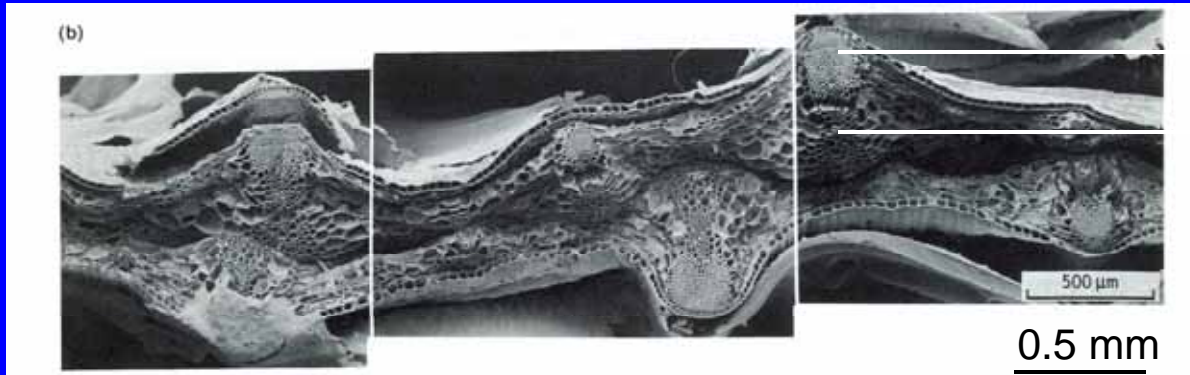


Iris



Bulrush

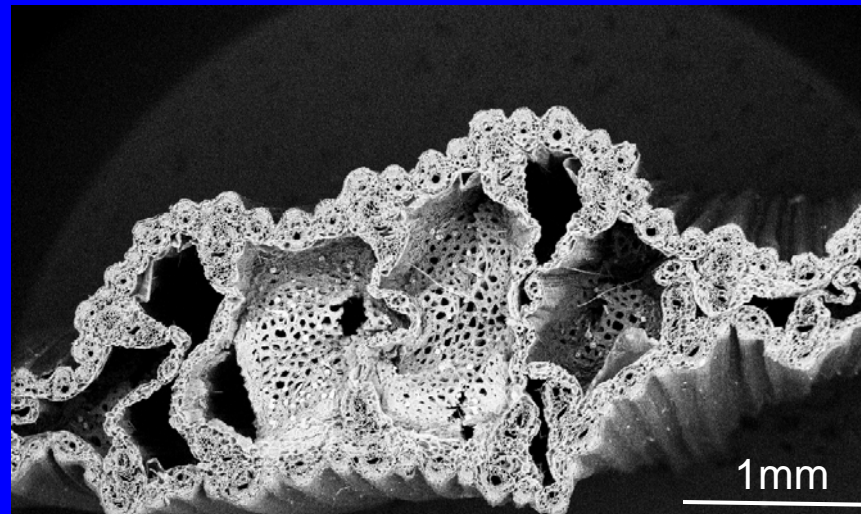
Sandwich Structures: Leaves



— Sclerenchyma

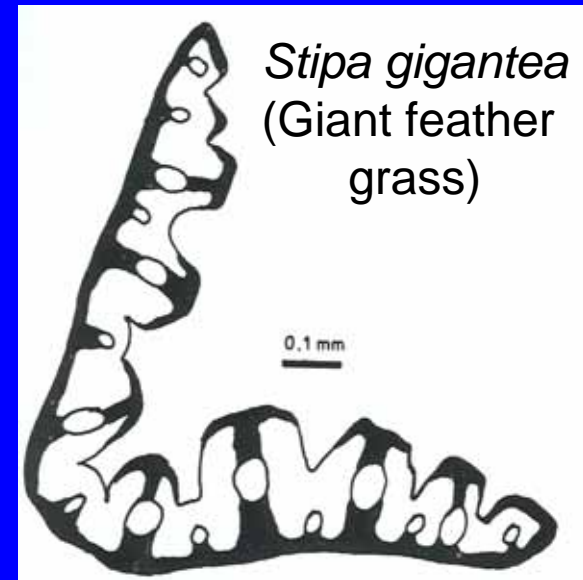
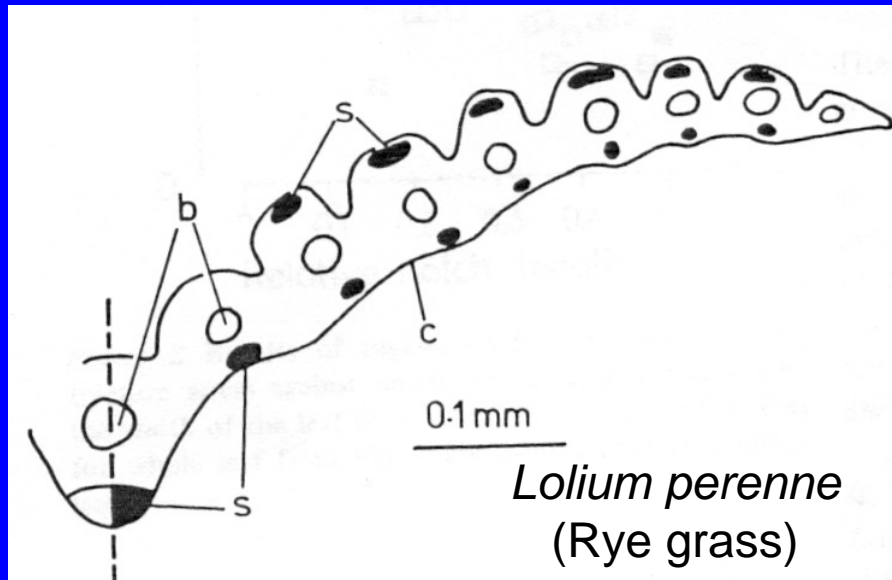
— Parenchyma

Iris leaf



Bulrush leaf

Sandwich Structures: Leaves



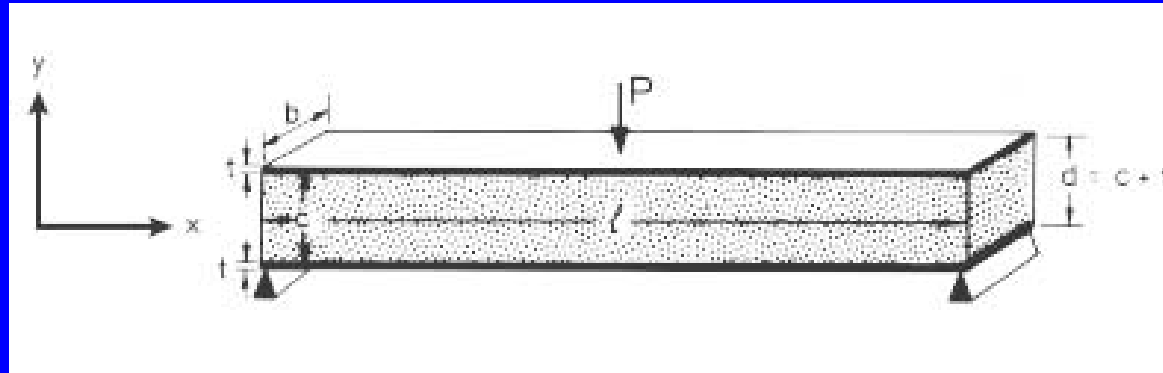
Black = sclerenchyma
White = parenchyma

Vincent, 1982,1991

Monocotyledon Leaves

- Fibers (sclerenchyma) along outer surface of leaves
- Foam-like cells (parenchyma) or ribs in core
- Acts like structural sandwich panel
- Increase in moment of inertia by separating stiff “faces” by a lightweight “core”
- Large surface area for photosynthesis

Sandwich Beam Deflection



$$\delta = \delta_b + \delta_s = \frac{Pl^3}{B_1 (EI)_{eq}} + \frac{Pl}{B_2 (AG)_{eq}}$$

Flexural rigidity: $(EI)_{eq} \approx \frac{E_f b t c^2}{2}$ Shear rigidity: $(AG)_{eq} \approx bcG_c$

Cantilever: $B_1 = 3$ $B_2 = 1$

Iris Leaves



$t = 30 \mu\text{m}$

$c = 0.5 \text{ to } 3.0 \text{ mm}$

$E_f = 8.2 \text{ GPa}$

$G_c = 2 \text{ MPa}$

Measured stiffnesses (N/mm):	0.66	0.54	0.41	0.25
Calculated stiffnesses (N/mm):	1.21	0.78	0.51	0.29
Calculated/measured:	1.83	1.44	1.24	1.16

Conclusion

- Wood
 - Uniform honeycomb increases $E^{1/2}/\rho$, $\sigma_f^{2/3}/\rho$
 - Constant ρ , E , σ_f , vary $r(z)$ in tree
- Palm stem
 - Radial density gradient
 - Constant r , vary $\rho(r)$, $E(r)$, $\sigma_f(r)$ in palm stem
 - Increases (EI) relative to uniform distribution of solid
 - Stress distribution across radius matches strength distribution

Conclusion

- Plant stems
 - Cylindrical shell with compliant core
 - Increases buckling resistance over equivalent hollow circular tube for large a/t
- Monocotyledon leaves
 - Sandwich structure, efficient in bending
 - Leaves provide own structural support as well as area for photosynthesis
 - Rectangular cross-section maximizes surface area for photosynthesis

Acknowledgements

- Mike Ashby, Ken Easterling, Hugh Shercliff
- Gebran Karam, Phoebe Cheng, Ulrike Wegst, Ros Olive, Tessa Shercliff
- Justin Breucop, Don Galler, Beth Beighlie
- National Science Foundation
- Matoula S. Salapatas Professorship at MIT

Image References

- Connor S (1994) *New England Natives: A celebration of people and trees*. Harvard University Press.
- Dinwoodie J (1981) *Timber: Its nature and behaviour*. Van Nostrand Reinhold.
- Rich PM (1987) Mechanical structure of the stem of arborescent palms. *Bot. Gazette* 148, 42.
- Rich PM (1987) Developmental anatomy of the stem of *Welfia Georgii*, *Iriarteia Gigantea* and other arborescent palms: Implications for mechanical support. *Am. J. Botany* 74, 792.